

Identifying and Controlling Risky Contingencies of Transmission Systems

Daniel Bienstock and Sean Harnett, Columbia University
Taedong Kim and Steve Wright, U. of Wisconsin

FERC Software conference, 2015

N - K criterion revisited

Previous work: Salmeron and Wood, Donde et al, Turitsyin, Hines

N - K criterion revisited

- N - 1 criterion widely used.

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

Table 1: $\binom{N}{K}$

N	$K = 2$	$K = 3$	$K = 4$
1000	499500	166167000	41417124750
4000	7998000	10658668000	10650673999000
8000	31996000	85301336000	170538695998000
10000	49995000	166616670000	416416712497500

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

Table 2: $\binom{N}{K}$

N	$K = 2$	$K = 3$	$K = 4$
1000	499500	166167000	41417124750
4000	7998000	10658668000	10650673999000
8000	31996000	85301336000	170538695998000
10000	49995000	166616670000	416416712497500

- It is too conservative. It is not conservative enough.

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

Table 3: $\binom{N}{K}$

N	$K = 2$	$K = 3$	$K = 4$
1000	499500	166167000	41417124750
4000	7998000	10658668000	10650673999000
8000	31996000	85301336000	170538695998000
10000	49995000	166616670000	416416712497500

- It is too conservative. It is not conservative enough.
 (T. Boston) during Hurricane Sandy, N - 142 was observed.

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

Table 4: $\binom{N}{K}$

N	$K = 2$	$K = 3$	$K = 4$
1000	499500	166167000	41417124750
4000	7998000	10658668000	10650673999000
8000	31996000	85301336000	170538695998000
10000	49995000	166616670000	416416712497500

- It is too conservative. It is not conservative enough.
(T. Boston) during Hurricane Sandy, N - 142 was observed.
- Perhaps N - K does not necessarily capture all interesting events?

Example: August 14 2003

U.S. - Canada report on blackout:

“Because it had been hot for several days in the Cleveland-Akron area, more air conditioners were running to overcome the persistent heat, and consuming relatively high levels of reactive power – further straining the area’s limited reactive generation capabilities.”

- A **system-wide** condition that impedes the system
- Not a cause, but a contributor
- Look for combined events ?

N - K criterion revisited

- N - 1 criterion widely used. But is it enough?
- How about N - K, for K “larger”? Everybody knows that:
 - It is *too* slow. A very difficult combinatorial problem.

Table 5: $\binom{N}{K}$

N	$K = 2$	$K = 3$	$K = 4$
1000	499500	166167000	41417124750
4000	7998000	10658668000	10650673999000
8000	31996000	85301336000	170538695998000
10000	49995000	166616670000	416416712497500

- It is too conservative. It is not conservative enough.
(T. Boston) during Hurricane Sandy, N - 142 was observed.
 - Perhaps N - K does not necessarily capture all interesting events?
- How can we deal with both types of problems?

A continuous interdiction model

- A fictitious adversary is trying to interdict the transmission system.
- This adversary negatively alters the physical parameters of equipment, e.g. transmission lines, so as to impede transmission.
- The adversary has a budget available (both system-wide and per-line).
 - On line km , reactance \mathbf{x}_{km} increased to $(1 + \lambda_{km})\mathbf{x}_{km}$

A continuous interdiction model

- A fictitious adversary is trying to interdict the transmission system.
- This adversary negatively alters the physical parameters of equipment, e.g. transmission lines, so as to impede transmission.
- The adversary has a budget available (both system-wide and per-line).
 - On line km , reactance x_{km} increased to $(1 + \lambda_{km})x_{km}$,
 - $0 \leq \lambda_{km} \leq \lambda_{km}^{max}$ (per line limit)

A continuous interdiction model

- A fictitious adversary is trying to interdict the transmission system.
- This adversary negatively alters the physical parameters of equipment, e.g. transmission lines, so as to impede transmission.
- The adversary has a budget available (both system-wide and per-line).
 - On line km , reactance x_{km} increased to $(1 + \lambda_{km})x_{km}$,
 - $0 \leq \lambda_{km} \leq \lambda_{km}^{max}$ (per line limit)
 - $\sum_{km} \lambda_{km} \leq \Lambda$ (global limit)

A continuous interdiction model

- A fictitious adversary is trying to interdict the transmission system.
- This adversary negatively alters the physical parameters of equipment, e.g. transmission lines, so as to impede transmission.
- The adversary has a budget available (both system-wide and per-line).
- Adversary maximizes the impact (e.g. voltage loss) over the available budget.
- A continuous, non-convex optimization problem with **simple** constraints.

No enumeration!

A blast from the past: Bienstock and Verma, 2007

- **DC approximation** to power flows.
- Adversary **increases reactances** of lines.
- **Limit** on total percentage-increase of reactances, and on per-line increase.
- Adversary maximizes the maximum **line overload**:

$$\max_{\mathbf{x}, \boldsymbol{\theta}} \max_{km} \left\{ \frac{|\theta_k - \theta_m|}{u_{km} \mathbf{x}_{km}} \right\}$$

$$\text{s.t.} \quad \mathbf{B}_{\mathbf{x}} \boldsymbol{\theta} = \mathbf{d}$$

\mathbf{x} within budget

- Variables: reactances \mathbf{x} , phase angles $\boldsymbol{\pi}$
 - \mathbf{x}_{km} = reactance of km , u_{km} = limit of km , $\mathbf{B}_{\mathbf{x}}$ = bus susceptance matrix, \mathbf{d} = net injections (given)
- Continuous, but non-smooth problem.

A blast from the past: Bienstock and Verma, 2007

- **DC approximation** to power flows.
- Adversary **increases reactances** of lines.
- **Limit** on total percentage-increase of reactances, and on per-line increase.
- Adversary maximizes the maximum **line overload**:

$$\begin{aligned} \max_{\mathbf{x}, \boldsymbol{\theta}} \quad & \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} \mathbf{x}_{km}} \\ \text{s.t.} \quad & \mathbf{B} \mathbf{x} \boldsymbol{\theta} = d \\ & \mathbf{x} \text{ within budget} \\ & \sum_{km} (\alpha_{km}^+ + \alpha_{km}^-) = 1, \quad \alpha^+, \alpha^- \geq 0. \end{aligned}$$

A blast from the past: Bienstock and Verma, 2007

- **DC approximation** to power flows.
- Adversary **increases reactances** of lines.
- **Limit** on total percentage-increase of reactances, and on per-line increase.
- Adversary maximizes the maximum **line overload**:

$$\begin{aligned} \max_{\mathbf{x}, \boldsymbol{\theta}, \boldsymbol{\alpha}} \quad & \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} \mathbf{x}_{km}} \\ \text{s.t.} \quad & \mathbf{B} \mathbf{x} \boldsymbol{\theta} = d \\ & \mathbf{x} \text{ within budget} \\ & \sum_{km} (\alpha_{km}^+ + \alpha_{km}^-) = 1, \quad \alpha^+, \alpha^- \geq 0. \end{aligned}$$

- Continuous, smooth, **nonconvex**.

Technical point

$$\begin{aligned}
 & \max_{\mathbf{x}, \boldsymbol{\theta}, \boldsymbol{\alpha}} \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} \mathbf{x}_{km}} \\
 & \text{s.t.} \quad \mathbf{B}_{\mathbf{x}} \boldsymbol{\theta} = d \\
 & \quad \mathbf{x} \text{ within budget} \\
 & \sum_{km} (\alpha_{km}^+ + \alpha_{km}^-) = 1, \quad \alpha^+, \alpha^- \geq 0.
 \end{aligned}$$

Function to maximize: $\mathbf{F}(\mathbf{x}, \boldsymbol{\alpha}) \doteq \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} x_{km}}$

Technical point

$$\begin{aligned} \max_{\mathbf{x}, \boldsymbol{\alpha}} \quad & \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} \mathbf{x}_{km}} \\ \text{s.t.} \quad & \mathbf{B}_{\mathbf{x}} \boldsymbol{\theta} = d \\ & \mathbf{x} \text{ within budget} \\ & \sum_{km} (\alpha_{km}^+ + \alpha_{km}^-) = 1, \quad \alpha^+, \alpha^- \geq 0. \end{aligned}$$

Function to maximize: $\mathbf{F}(\mathbf{x}, \boldsymbol{\alpha}) \doteq \sum_{km} (\alpha_{km}^+ - \alpha_{km}^-) \frac{(\theta_k - \theta_m)}{u_{km} x_{km}}$

- **Fact:** The gradient and the Hessian of $F(x, \alpha)$ can be efficiently computed
- Optimization problem solved using **LOQO** (**IPOPT** an option)

And what happens?

- Algorithm scales well (2007): CPU times of ~ 1 hour for studying systems with thousands of lines.

And what happens?

- Algorithm scales well (2007): CPU times of ~ 1 hour for studying systems with thousands of lines.
- Optimal * attack concentrated on a handful of lines

And what happens?

- Algorithm scales well (2007): CPU times of ~ 1 hour for studying systems with thousands of lines.
- Optimal * attack concentrated on a handful of lines
- Significant part of the budget expended on many lines, with visible impact

Table 6: Attack patterns

single = 20 total = 60		single = 10 total = 30		single = 10 total = 40	
Range	Count	Range	Count	Range	Count
[1, 1]	8	[1, 1]	1	[1, 1]	14
(1, 2]	72	(1, 2]	405	(1, 2]	970
(2, 3]	4	(2, 9]	0	(2, 5]	3
(5, 6]	1	(9, 10]	3	(5, 6]	0
(6, 7]	1			(6, 7]	1
(7, 8]	4			(7, 9]	0
(8, 20]	0			(9, 10]	2

“single” = max multiplicative increase of a line’s reactance

“total” = max total multiplicative increase of line reactances

Today: the AC power flows setting

As before, adversary increases impedances, subject to budgets

Adversary wants to **maximize:**

- Phase angle differences across ends of a lines
- Voltage deviations (loss)

Alternative version:

- There is a **recourse** action: shed load so as to maintain feasibility of all power flow constraints (limits)
- Adversary wants to maximize the amount of lost load

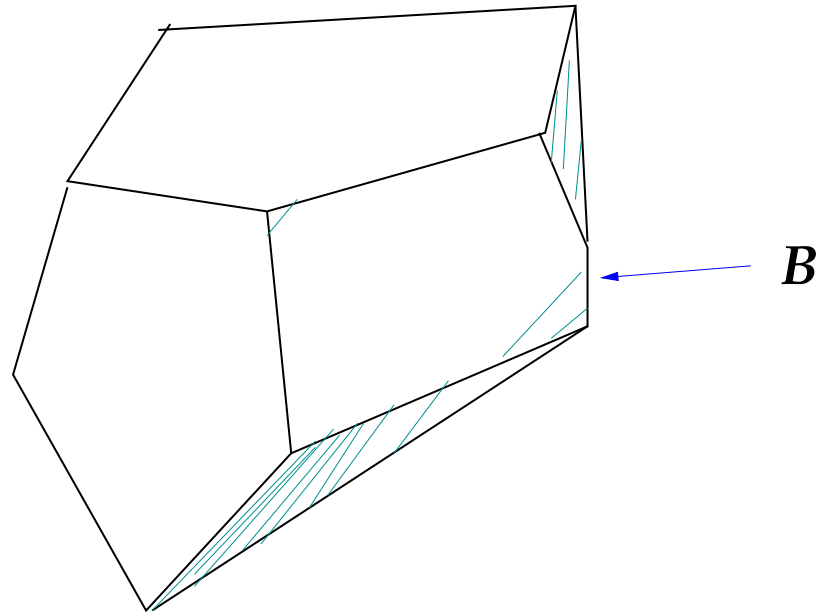
Generically:

$$\begin{array}{ll} \mathbf{max} & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \end{array}$$

- \mathbf{x} = impedances, \mathcal{B} = budget constraints
- $\mathcal{F}(\mathbf{x})$ = measure of phase angle differences, voltage loss, load loss
- Challenge 1: $\mathcal{F}(\mathbf{x})$ is implicitly defined

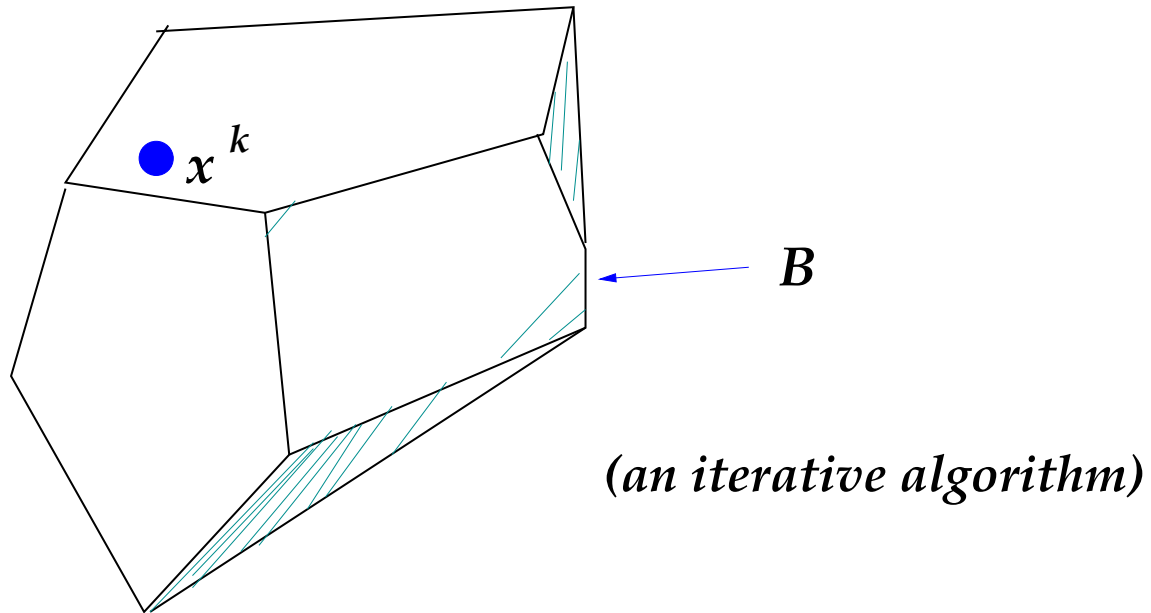
Basic methodology: **Frank-Wolfe**

$$\begin{array}{ll}\max & \mathcal{F}(\boldsymbol{x}) \\ \text{s.t.} & \boldsymbol{x} \in \mathcal{B} \quad (\text{within budget})\end{array}$$



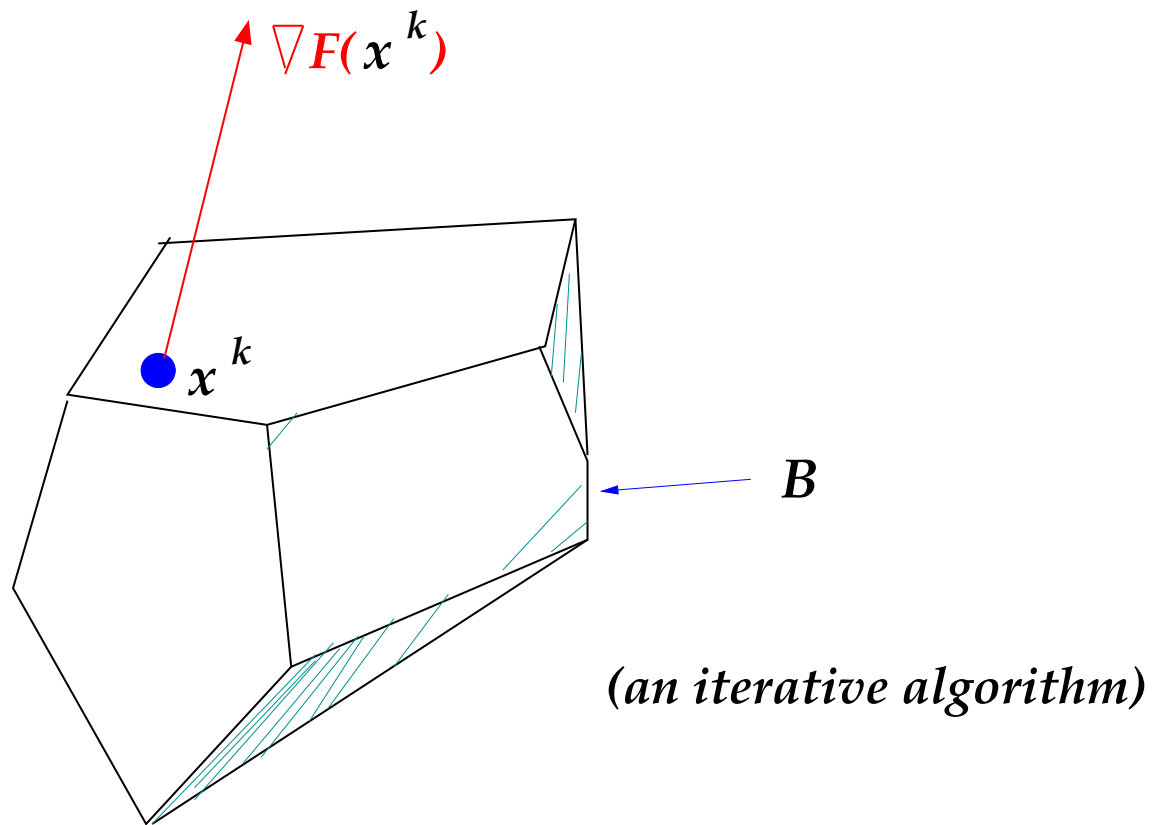
Basic methodology: **Frank-Wolfe**

$$\begin{array}{ll} \max & \mathcal{F}(x) \\ \text{s.t.} & x \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



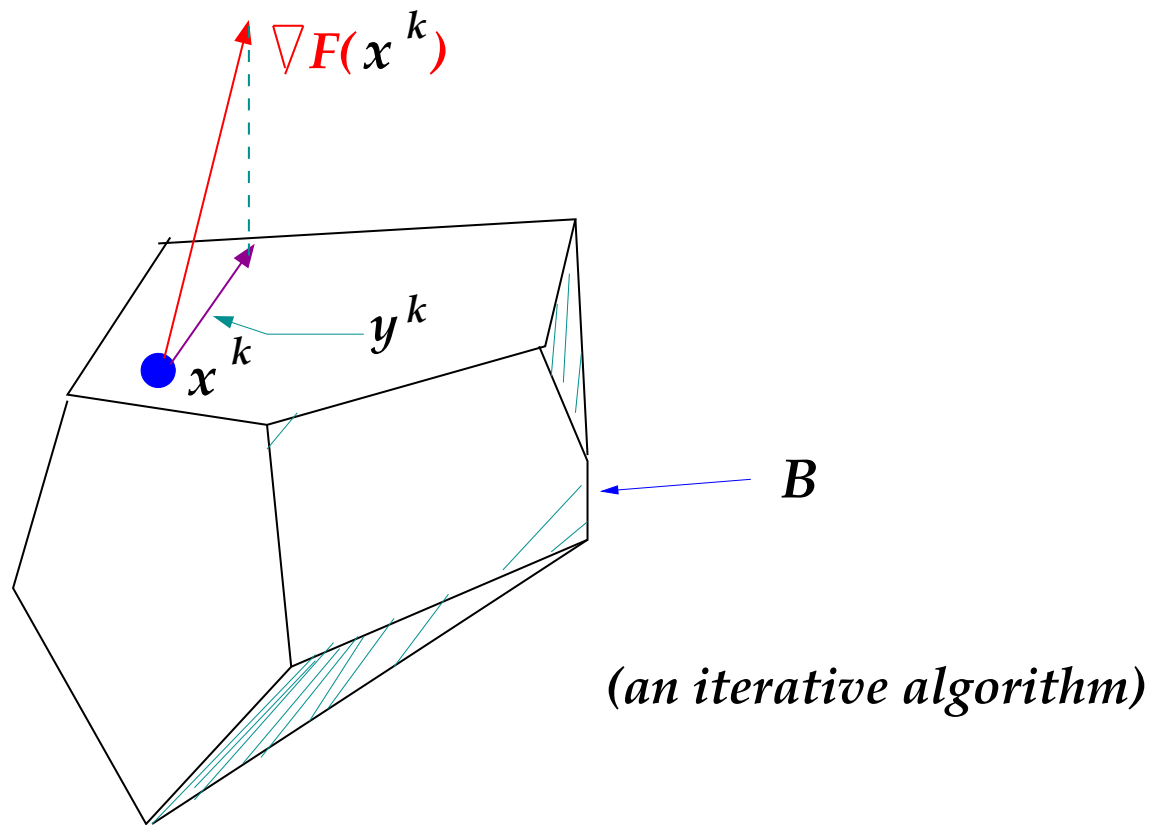
Basic methodology: **Frank-Wolfe**

$$\begin{array}{ll} \max & \mathcal{F}(x) \\ \text{s.t.} & x \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



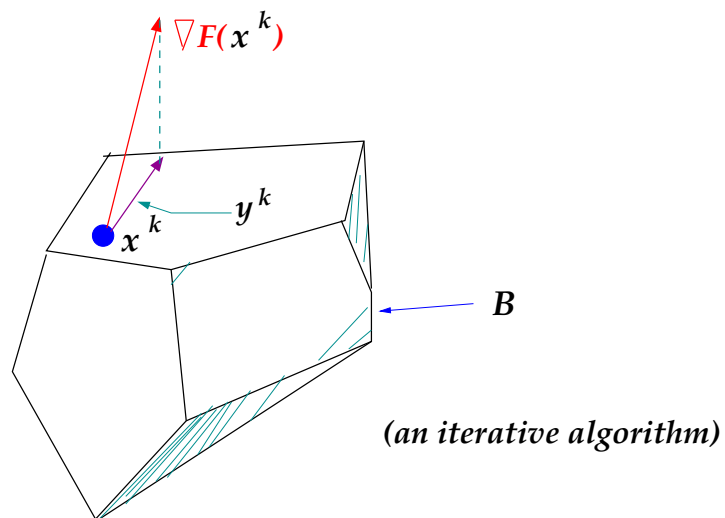
Basic methodology: **Frank-Wolfe**

$$\begin{array}{ll} \max & \mathcal{F}(x) \\ \text{s.t.} & x \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



Basic methodology: **Frank-Wolfe**

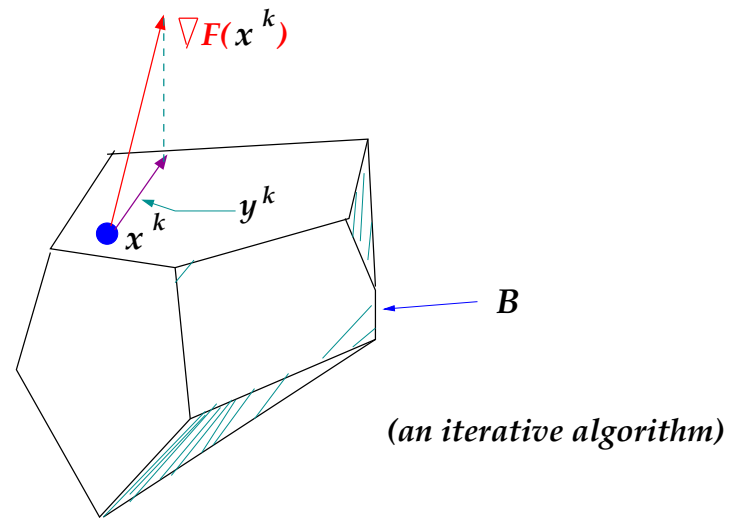
$$\begin{array}{ll} \max & \mathcal{F}(x) \\ \text{s.t.} & x \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



$$y^k \text{ solves } \begin{array}{ll} \max & [\nabla \mathcal{F}(x^k)]^T y \\ \text{s.t.} & x^k + y \in \mathcal{B} \quad (\text{within budget}) \end{array}$$

Basic methodology: **Frank-Wolfe**

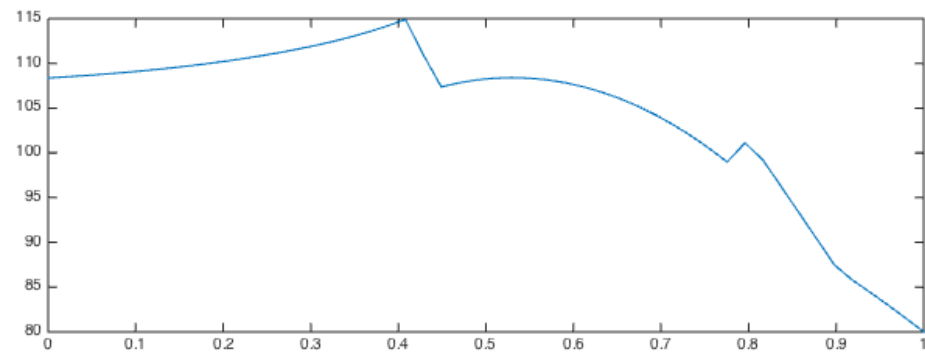
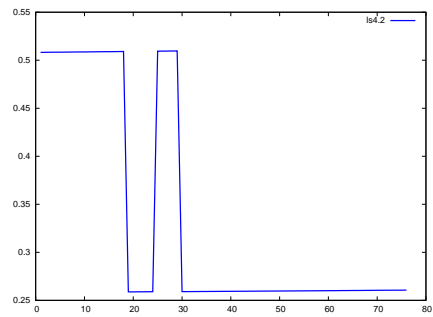
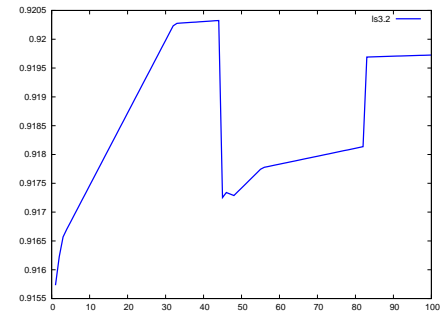
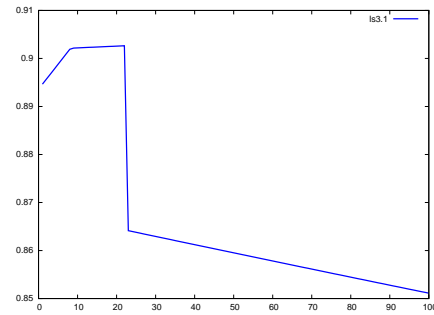
$$\begin{array}{ll} \max & \mathcal{F}(x) \\ \text{s.t.} & x \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



$$y^k \text{ solves } \begin{array}{ll} \max & [\nabla \mathcal{F}(x^k)]^T y \\ \text{s.t.} & x^k + y \in \mathcal{B} \quad (\text{within budget}) \end{array}$$

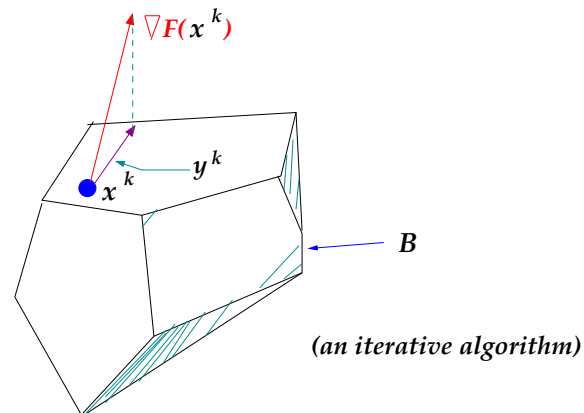
Final step is a **line search**: $x^{k+1} = x^k + \alpha y^k$, where $0 \leq \alpha \leq 1$ is the stepsize.

Line searches



Challenge 2

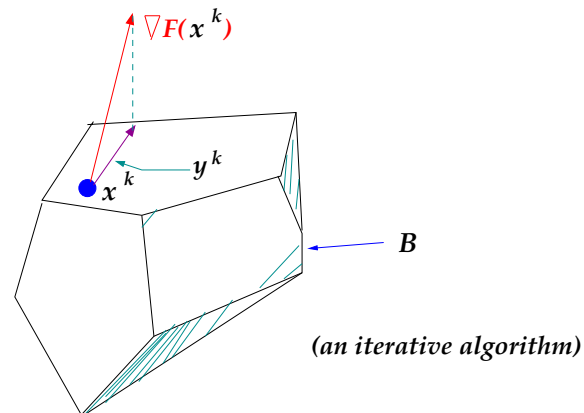
$$\begin{array}{ll} \max & \mathcal{F}(\boldsymbol{x}) \\ \text{s.t.} & \boldsymbol{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- Recall: $\mathcal{F}(\boldsymbol{x})$ measures e.g. the largest phase angle difference using reactances \boldsymbol{x}
- Q: exactly how do we get $\nabla \mathcal{F}(\boldsymbol{x})$?

Challenge 2

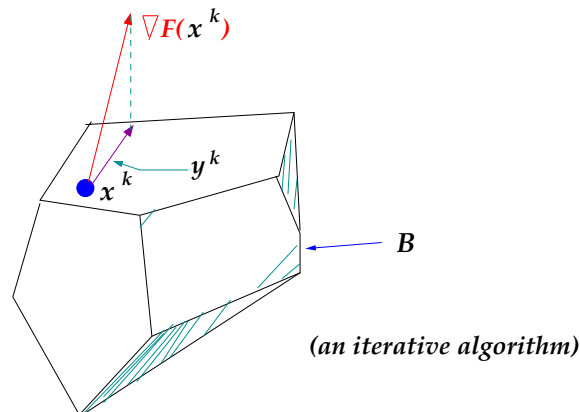
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- Recall: $\mathcal{F}(\mathbf{x})$ measures e.g. the largest phase angle difference using reactances \mathbf{x}
- **Q:** exactly how do we get $\nabla \mathcal{F}(\mathbf{x})$?
- **A:** We estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences

Challenge 2

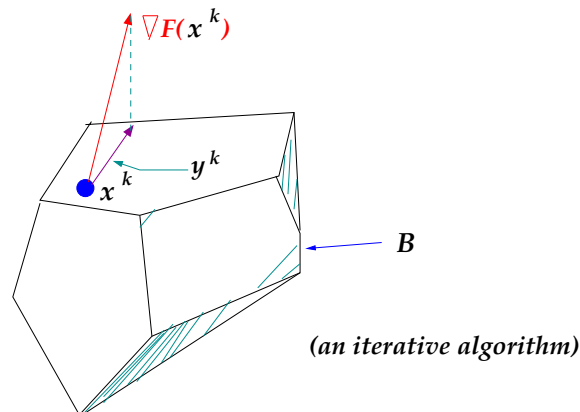
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- Recall: $\mathcal{F}(\mathbf{x})$ measures e.g. the largest phase angle difference using reactances \mathbf{x}
- **Q:** exactly how do we get $\nabla \mathcal{F}(\mathbf{x})$?
- **A:** We estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- But $\nabla \mathcal{F}(\mathbf{x})$ is a vector with an entry for each line of the transmission system – it is a **big** vector

Challenge 2

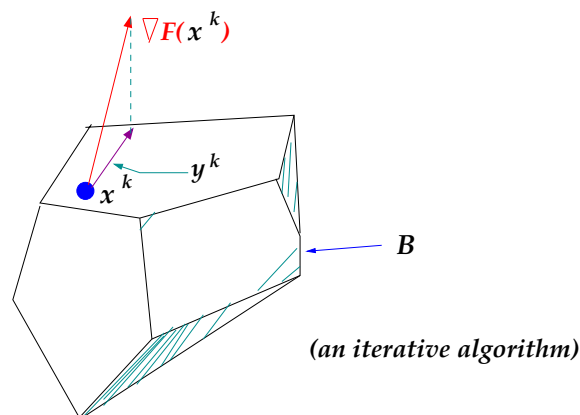
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- Recall: $\mathcal{F}(\mathbf{x})$ measures e.g. the largest phase angle difference using reactances \mathbf{x}
- **Q:** exactly how do we get $\nabla \mathcal{F}(\mathbf{x})$?
- **A:** We estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- But $\nabla \mathcal{F}(\mathbf{x})$ is a vector with an entry for each line of the transmission system – it is a **big** vector
- **“Solution”:** Estimate $\nabla \mathcal{F}(\mathbf{x})$ in parallel over several cores

Challenge 2

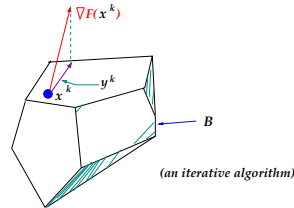
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- Recall: $\mathcal{F}(\mathbf{x})$ measures e.g. the largest phase angle difference using reactances \mathbf{x}
- **Q:** exactly how do we get $\nabla \mathcal{F}(\mathbf{x})$?
- **A:** We estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- But $\nabla \mathcal{F}(\mathbf{x})$ is a vector with an entry for each line of the transmission system – it is a **big** vector
- **“Solution”:** Estimate $\nabla \mathcal{F}(\mathbf{x})$ in parallel over several cores
- **Alternative:** only estimate some of the components of $\nabla \mathcal{F}(\mathbf{x})$:
 - **Random** subset of small size
 - **Most promising** subset

Challenge 3

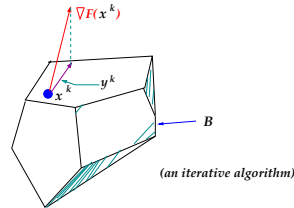
$$\begin{array}{ll}\max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget})\end{array}$$



- $\mathcal{F}(\mathbf{x})$ measures e.g. the sum of voltage losses with reactances \mathbf{x}
- And we estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- Q: How do we compute $\mathcal{F}(\mathbf{x})$, for given reactances \mathbf{x} ?

Challenge 3

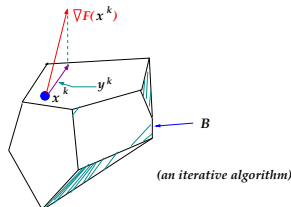
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- $\mathcal{F}(\mathbf{x})$ measures e.g. the sum of voltage losses with reactances \mathbf{x}
- And we estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- **Q:** How do we compute $\mathcal{F}(\mathbf{x})$, for given reactances \mathbf{x} ?
- **A:** Ideally, a **PF** (load flow) calculation

Challenge 3

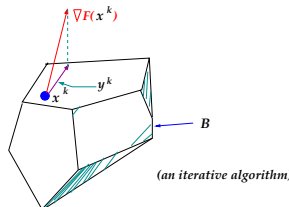
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- $\mathcal{F}(\mathbf{x})$ measures e.g. the sum of voltage losses with reactances \mathbf{x}
- And we estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- **Q:** How do we compute $\mathcal{F}(\mathbf{x})$, for given reactances \mathbf{x} ?
- **A:** Ideally, a **PF** (load flow) calculation
- **Challenge!** PF **often does not converge** for interesting \mathbf{x}

Challenge 3

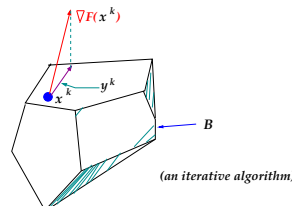
$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- $\mathcal{F}(\mathbf{x})$ measures e.g. the sum of voltage losses with reactances \mathbf{x}
- And we estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- **Q:** How do we compute $\mathcal{F}(\mathbf{x})$, for given reactances \mathbf{x} ?
- **A:** Ideally, a **PF** (load flow) calculation
- **Challenge!** PF **often does not converge** for interesting \mathbf{x}
- **solution:** solution OPF-like problem:
minimize sum of square of all violations (load mismatch, line limits, etc)

Challenge 3

$$\begin{array}{ll} \max & \mathcal{F}(\mathbf{x}) \\ \text{s.t.} & \mathbf{x} \in \mathcal{B} \quad (\text{within budget}) \end{array}$$



- $\mathcal{F}(\mathbf{x})$ measures e.g. the sum of voltage losses with reactances \mathbf{x}
- And we estimate $\nabla \mathcal{F}(\mathbf{x})$ using finite differences
- **Q:** How do we compute $\mathcal{F}(\mathbf{x})$, for given reactances \mathbf{x} ?
- **A:** Ideally, a **PF** (load flow) calculation
- **Challenge!** PF **often does not converge** for interesting \mathbf{x}
- **solution:** solution OPF-like problem:
minimize sum of square of all violations (load mismatch, line limits, etc)
- **solution?** violations still observed
- **solution?** Add to definition of $\mathcal{F}(\mathbf{x})$ sum of weighted square violations
- Currently using **IPOPT** within Matpower (fastest for **our** purposes)
- Infeasible cases verified using SDP relaxation

Example: phase angle attack on Polish grid (from Matpower)

1 obj=2620.72 step=1.00 [**263** 8.00; **300** 8.00; **728** 8.00;]

2 obj=2641.52 step=1.00 [**305** 8.00; **306** 8.00; **309** 8.00;]

3 obj=2649.34 step=1.00 [**168** 8.00; **263** 8.00; **321** 8.00;]

5 obj=2765.47 step=0.50 [**51** 4.00; **261** 4.00; **263** 4.00; **300** 4.00; **321** 4.00; **322** 4.00;]

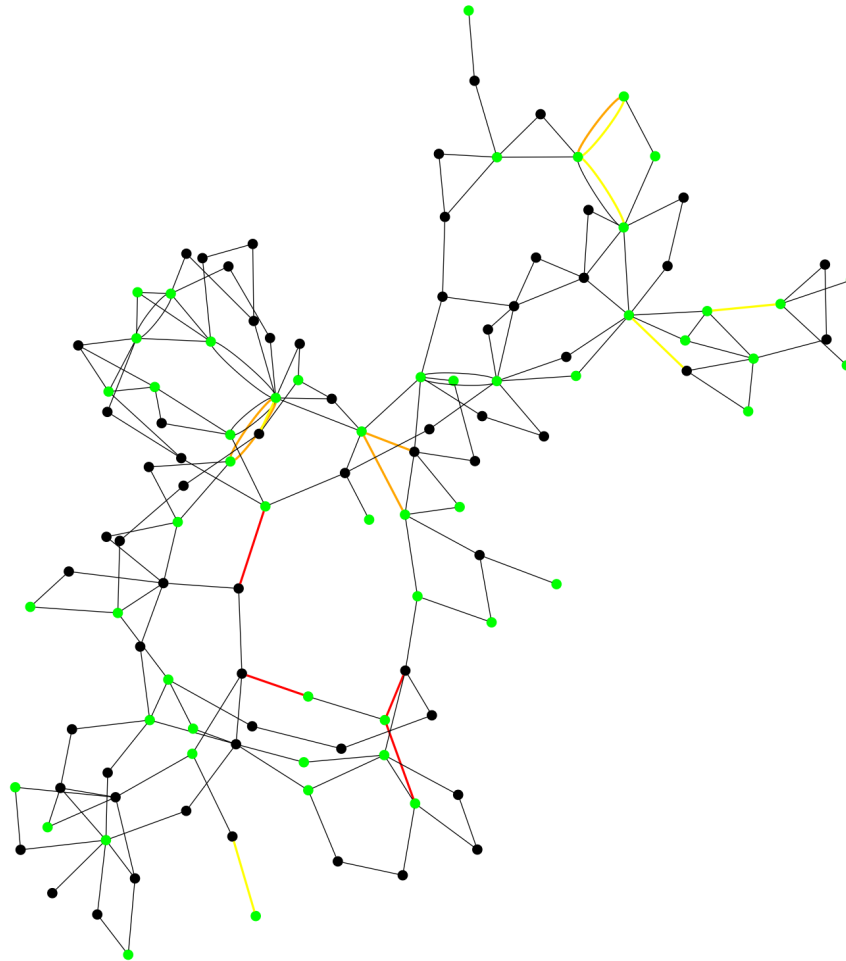
13 obj=2944.01 step=0.12 [**305** 2.60; **168** 2.32; **322** 2.17; **169** 1.90; **321** 1.85; **263** 1.57; **309** 1.50; **32** 1.15; **51** 1.08; **261** 1.08; **170** 1.00; **171** 1.00; **306** 0.85; **39** 0.75; **281** 0.75; **166** 0.57; **310** 0.57; **8** 0.43; **264** 0.43; **300** 0.42;]

20 obj=2950.54 step=0.03 [**169** 2.53; **305** 2.38; **168** 1.88; **322** 1.77; **321** 1.76; **309** 1.74; **166** 1.44; **170** 1.28; **263** 1.28; **261** 1.14; **32** 0.93; **51** 0.88; **171** 0.81; **306** 0.69; **39** 0.61; **281** 0.61; **264** 0.59; **260** 0.51; **310** 0.46; **8** 0.35; **300** 0.34;]

27 obj=2958.08 **step=0.00** [**169** 2.80; **305** 2.53; **321** 2.00; **309** 1.97; **168** 1.63; **263** 1.58; **322** 1.53; **166** 1.38; **261** 1.11; **170** 1.11; **32** 0.81; **51** 0.76; **264** 0.76; **281** 0.75; **171** 0.71; **306** 0.60; **39** 0.53; **260** 0.44; **310** 0.40; **8** 0.30; **300** 0.30;]

Example: phase angle attack on 118-bus

Three top-attacked lines in red:



Fact: phase angle attack cannot be isolated to a few lines

Fact: phase angle attack cannot be isolated to a few lines

Experiment on 118-bus case:

- (1) Take line most heavily interdicted: line **38**
- (2) Let the reactance of this line increase to infinity
- (3) What happens? Phase angle difference $\rightarrow \pi/2$?

Fact: phase angle attack cannot be isolated to a few lines

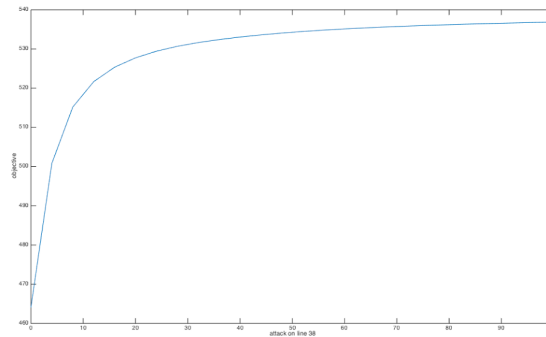
Experiment on 118-bus case:

- (1) Take line most heavily interdicted: line **38**
- (2) Let the reactance of this line increase to infinity
- (3) What happens? Phase angle difference $\rightarrow \pi/2$? **No.**

Fact: phase angle attack cannot be isolated to a few lines

Experiment on 118-bus case:

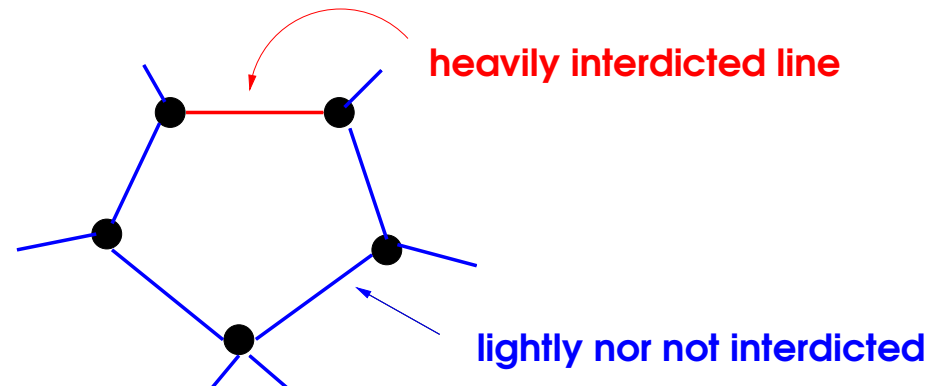
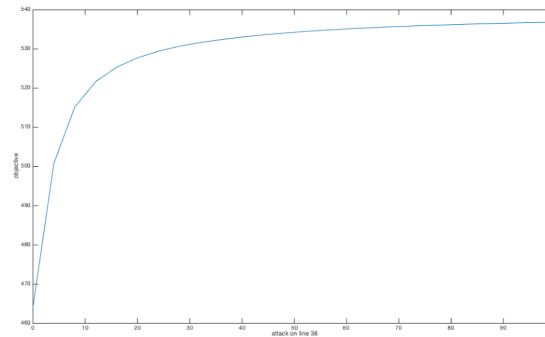
- (1) Take line most heavily interdicted: line **38**
- (2) Let the reactance of this line increase to infinity
- (3) What happens? Phase angle difference $\rightarrow \pi/2$? **No.**
From ≈ 10 to ≈ 40 .



Fact: phase angle attack cannot be isolated to a few lines

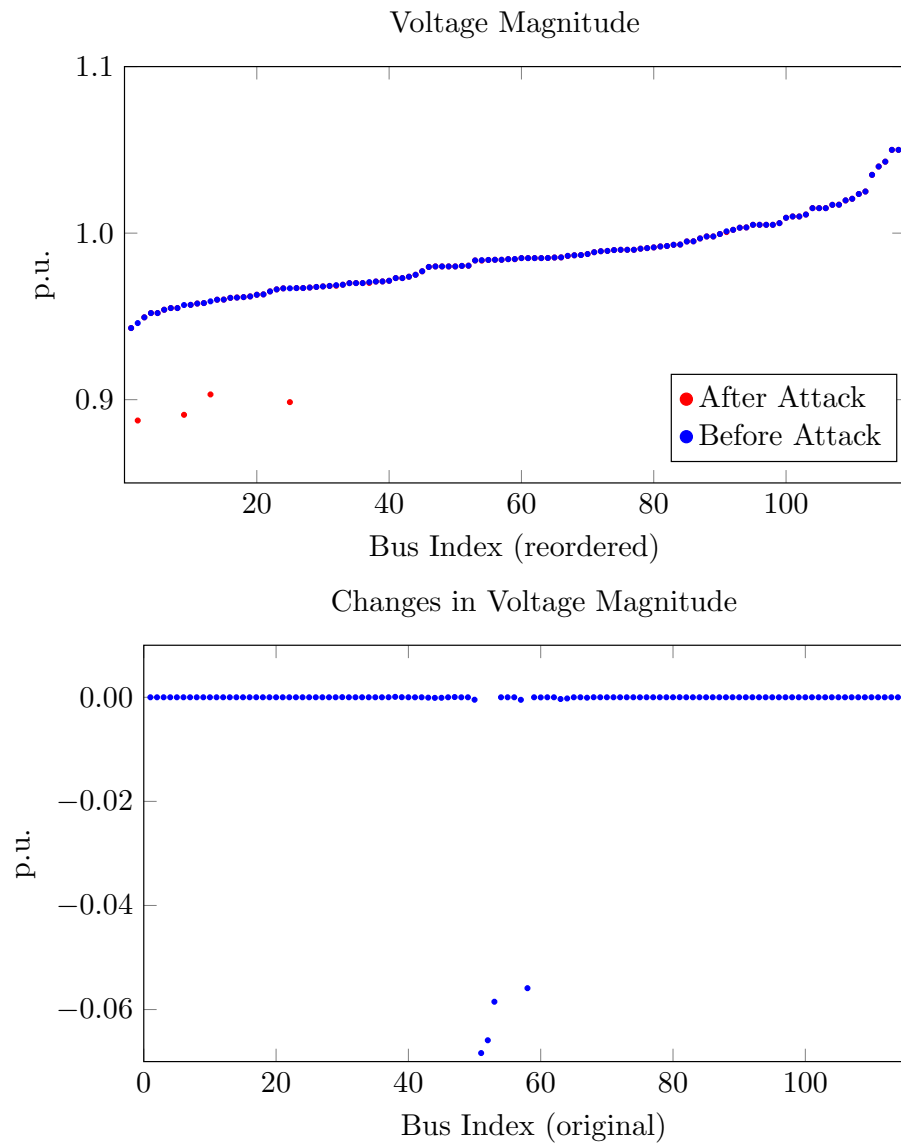
Experiment on 118-bus case:

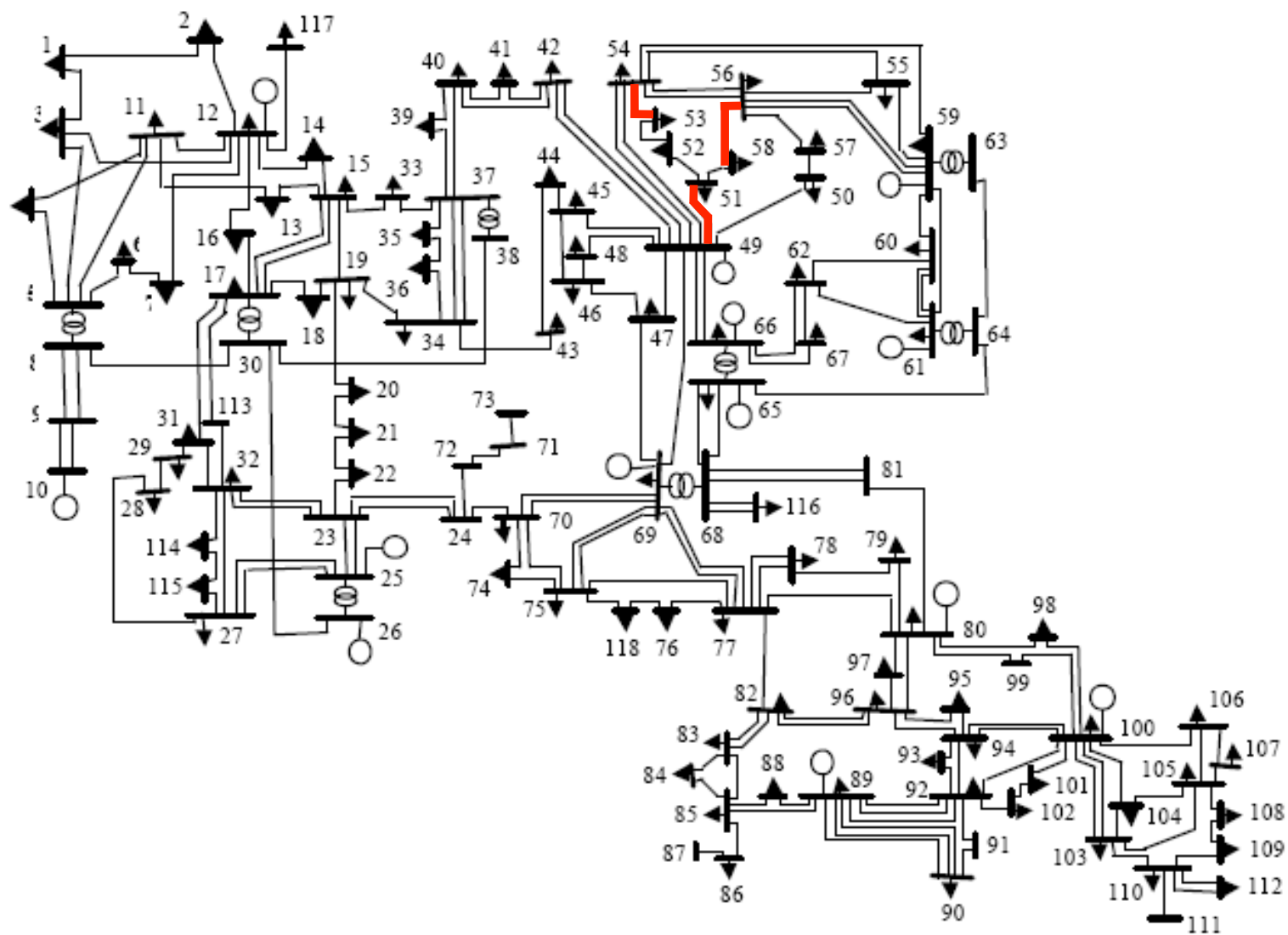
- (1) Take line most heavily interdicted: line **38**
- (2) Let the reactance of this line increase to infinity
- (3) What happens? Phase angle difference $\rightarrow \pi/2$? **No.**
From ≈ 10 to ≈ 40 .



Voltage attack on 118-bus

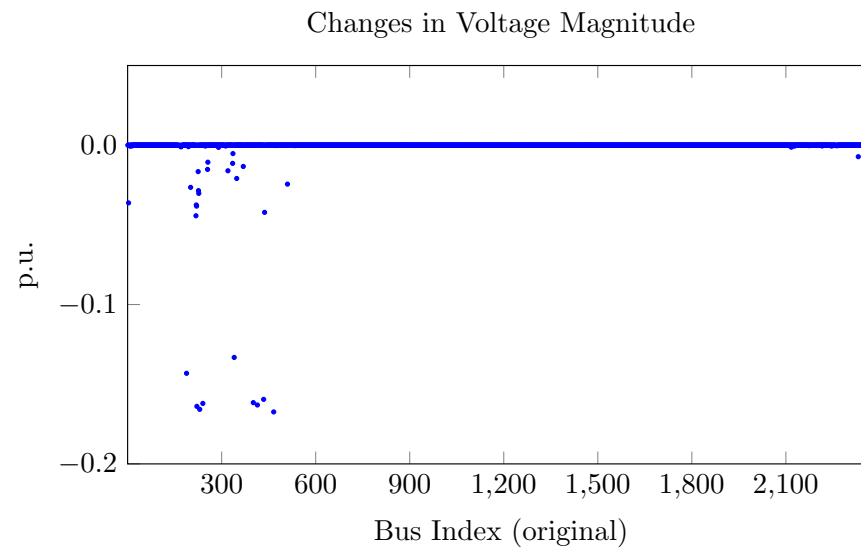
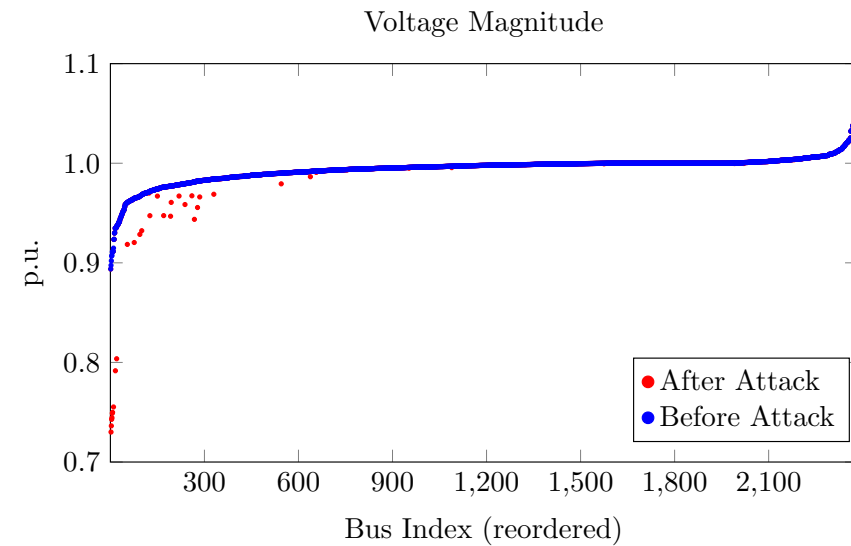
“Triple the reactance of at most three lines”





Voltage attack on 2383-bus Polish

“Double the reactance of at most three lines”



→ Primarily 4 lines interdicted