A Multi-Period OPF Approach to Improve Voltage Stability using Demand Response

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Power System Stability

- Frequency instability
 - Associated with an imbalance between load and generation
 - Demand response based on temporal shifting of load

[Short, Infield, & Freris '07], [Molina-Garcia, Bouffard, & Kirschen '10], [Mathieu, Koch, & Callaway '12], [Zhang, Lian, Chang, & Kalsi '13]

- Voltage instability
 - Associated with operation that nears the limits of the network's power transfer capability
 - Demand response based on spatial shifting of load

How to control flexible loads in order to improve voltage stability after a disturbance?



Voltage Stability

- Distance to the "nose point" of the PV curve
 - Often computed using continuation methods, which are difficult to embed within an optimization problem
 - A voltage stability metric based on power flow sensitivities is based on the smallest singular value of the power flow Jacobian [Tiranuchit & Thomas '88], [Lof, Smed, Andersson, & Hill '92]



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Our Approach

- Maximize the smallest singular value of the power flow Jacobian via control of flexible load demands
- Spatial shifting of loads with total demand held constant over time to maintain frequency stability







Post-disturbance operating point











Problem Formulation





Assumptions

- Load models
 - Constant power factor
 - Flexible loads at some or all PQ buses
 - Total demand from flexible loads held constant at each period
- Generator models
 - Modeled as PV buses immediately after the disturbance
 - Active power generation redispatched in subsequent periods

We first show the single-period formulation, and then extend to a multi-period setting.



Smallest Singular Value Maximization

 $\max \lambda_0$

subject to

 $\mathcal{F}\left(x\right) = 0$

Formulation

 $\mathbf{J}\,(\theta,V)^{\intercal}\,\mathbf{J}\,(\theta,V) - \lambda_0\,\mathbf{I} \succeq 0 \qquad \lambda_0 \leq \underset{\text{the power flow Jacobian}}{\text{smallest singular value of}}$

$$\sum_{i \in \mathcal{S}_{DR}} P_{d,i} = P_{d,total}$$
 Total flexible load demand is constant

AC power flow equations

 $\mathcal{G}(x) \ge 0$ Operational limits $x = \{P_q, Q_q, P_d, Q_d, V, \theta\}$

Directly solving this problem is challenging

Similar to the formulations in [Berizzi et al. '01], [Cañizares et al. '01]



Solution via Successive Linearization

- Use singular value sensitivities and a linearization of the AC power flow equations
- Sensitivity of the singular values λ_i for the Jacobian $\mathbf{J}(\xi)$ with respect to a parameter in $\xi = \begin{bmatrix} \theta_1 & \dots & \theta_n & V_1 & \dots & V_n \end{bmatrix}^{\mathsf{T}}$:

$$\frac{\partial \lambda_i}{\partial \xi} = \underbrace{w_i^{\mathsf{T}}}_{\mathbf{i}} \frac{\partial \left((\mathbf{J} (\xi))^{\mathsf{T}} \mathbf{J} (\xi) \right)}{\partial \xi} \underbrace{u_i}_{\mathbf{k} \in \mathsf{I}}$$
Left eigenvector Right eigenvector
The approximate change in λ_0 is

$$\Delta \lambda_0 = \sum_{i=1}^n \left[w_0^{\mathsf{T}} \frac{\partial \left((\mathbf{J} (\xi))^{\mathsf{T}} \mathbf{J} (\xi) \right)}{\partial \theta_i} u_0 \right] \Delta \theta_i + \left[w_0^{\mathsf{T}} \frac{\partial \left((\mathbf{J} (\xi))^{\mathsf{T}} \mathbf{J} (\xi) \right)}{\partial V_i} u_0 \right] \Delta V_i$$



Incremental Formulation

 $\begin{array}{ll} \max & \Delta \lambda_0 \\ \text{subject to} \end{array}$

 $\sum \Delta P_{d,i} = 0$

 $i \in S_{DR}$

 $\begin{aligned} f(\Delta x) &= 0\\ g(\Delta x) \geq 0 \end{aligned}$

Take a step that seeks to increase the smallest singular value

$$\Delta \lambda_0 = \sum_{i=1}^n \left[w_0^{\mathsf{T}} \frac{\partial \left((\mathbf{J} \left(\xi \right))^{\mathsf{T}} \mathbf{J} \left(\xi \right) \right)}{\partial \theta_i} u_0 \right] \Delta \theta_i + \left[w_0^{\mathsf{T}} \frac{\partial \left((\mathbf{J} \left(\xi \right))^{\mathsf{T}} \mathbf{J} \left(\xi \right) \right)}{\partial V_i} u_0 \right] \Delta V_i$$

The singular value sensitivity

Total flexible load demand is constant

Linearized AC power flow equations

Linearized operational constraints

See [Yao, Mathieu, & Molzahn '17] for the full formulation.



Successive Linearization Algorithm





Recall the Multi-Period Approach



Recall the Multi-Period Approach





Multi-Period Formulation

$$\min_{\mathbf{x}(t)} \quad -\alpha \,\lambda_0(1) + \beta \,\mathcal{C}\left(P_G(2)\right)$$

subject to

$$\mathbf{J}(t)^{\mathsf{T}}\mathbf{J}(t) - \lambda_0(t)\mathbf{I} \succeq 0$$

$$\sum_{i \in \mathcal{S}_{DR}} P_{d,i}(1) = P_{d,total}$$

$$P_{d,i}(1) + P_{d,i}(2) = P_{d,i}^{\circ}, \ \forall i \in \mathcal{S}_{DR}$$

 $\mathcal{F}(x(t)) = 0, \quad \mathcal{G}(x(t)) \ge 0$

Optimize a weighted sum of the smallest singular value and the generation redispatch cost for energy payback

 $\lambda_0(t) \leq \mathop{\rm smallest\ singular\ value\ of}_{\rm the\ power\ flow\ Jacobian}$

Total flexible load demand is constant

Power demand shifted from flexible loads is "paid back"

AC power flow equations and operational limits

t=1: Smallest singular value maximization t=2: Energy payback for flexible loads



Multi-Period Formulation

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subject to

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AC power flow equations and operational limits

Solve using a successive linearization algorithm



Test Cases





Nine-Bus Test Case



59% decrease

Test Cases



Results: Smallest Singular Value





Results: Generation Cost



0.8% increase in generation cost from spatially shifting controllable loads

Test Cases



Convergence Rate



The successive linear programming algorithm typically converges in a few tens of iterations





Trade-Off Between Smallest Singular Value and Generation Cost



The weights in the objective function effectively control the trade-off between higher generation cost and improved voltage stability margins



Test Cases

IEEE 118-Bus Test Case



IEEE 118-Bus Test Case



Conclusion



Conclusion

- Spatial shifting of load can improve voltage stability margins after a disturbance
- To determine appropriate load control, we formulated a multi-period optimization problem and applied a successive linearization solution algorithm
- Future work:
 - Incorporating more detailed load models (ZIP loads)
 - Improving computational speed
 - Characterizing closeness to global optimality using convex relaxation techniques



Questions?

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margin problem generator engineering system assume advanced non-convex instability eigenvalue consumption equations shows demand including magnitudes flexible shown slack margins optimal loads imit goal while approach maximum pattern basic time reactive actions change compute response sults increases real MW size step algorithm

distance different buses DR initial function Future time reactive actions change compute response results increases real MW size step algorithm factor matrix near solve systems AC sensitivities represent maximize SSV limits line PQ singular brute **PV** force solution linear operating possible deneration associated point total bus paper model zation solutions value voltage **IO** constraints Jacobian method constant iterative midefinite maximizina load approaches magnitude maximizes convergence smallest

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