

# Strengthened MILP Formulation for the Edge-based Combined-Cycle Unit Model

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Joint work with  
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# Outline

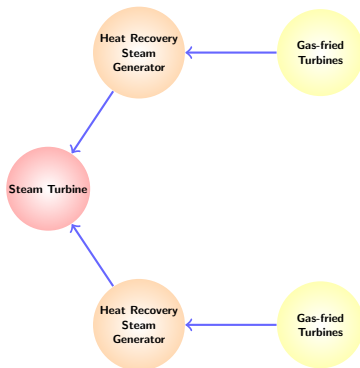
- 1 Introduction
  - Introduction
  - Motivation
- 2 Edge-Based Formulation
  - Transition Graph Representation
  - Operating Constraints
- 3 Strengthened Edge-Based Formulation
  - Tighter Constraints
  - Strong Valid Inequalities
- 4 Case Studies
- 5 Conclusion

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# Combined-Cycle Units

- Combustion Turbines: use natural gas, produce electricity and heat.
- Heat Recovery Steam Generator: produce steam.
- Steam Turbines: use steam to produce electricity.



# Current Practice

- Aggregated modeling approach [1]:
  - Treats the whole combined-cycle unit as a traditional thermal unit.
  - Less decision variables.
  - Cannot reflect the relationship between CT and ST.
- Pseudo unit approach [2]:
  - Associates each combustion turbine (CT) with a portion of the steam turbine (ST).
  - Less decision variables.
  - Cannot capture the transition process.
- Configuration-based model [3],[4],[5],[6]:
  - Represents each combination of CTs and STs as a configuration.
  - Cannot capture the operating constraints such as min-up/-down constraints for each turbine.

# Configuration-Based Model

- Work at different typical configurations: 0CT + 0ST, 1CT + 0ST, 2CTs + 0ST, 1CT + 1ST, and 2CTs + 1ST
- Each configuration is treated as a pseudo unit: generation limits, ramping rates, and min-up/-down constraints.

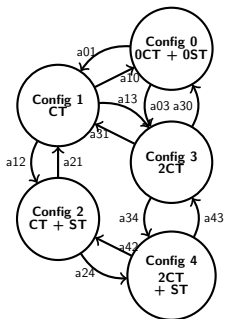


Figure: Transition Graph for 2CTs + 1ST

# Challenges

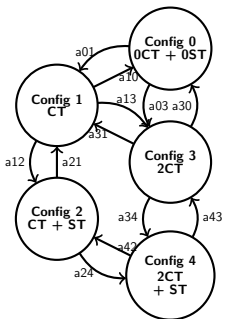
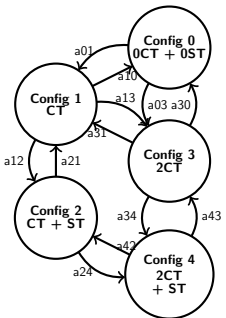


Figure: Transition Graph for 2CTs + 1ST

- Time  $t$ , Configuration 1 online
- Time  $t + 2$  Load increases, Generation amount increases, ST starts up, Configuration 2 online
- Time  $t + 3$  Works at Configuration 2 for several time periods (e.g., 4 time periods).
- If load increases dramatically, it might be more than the capacity of Configuration 2 at time  $t + 3, t + 4$ .
- Second CT can start up, if this CT satisfies its own min-down time requirement.

# Challenges



- Improve flexibility?
- Design the min-up/-down constraints for each turbine instead of each configuration.

Figure: Transition Graph for 2CTs + 1ST



# Edge-Based Combined-Cycle Unit Model

## ■ Motivation

- Improved the accuracy of the configuration-based model [7].

## ■ Method

- Proposed an edge-based formulation based on the transition graph.

## ■ Contribution

- Exactly described the physical constraints (in particular, min-up/-down restrictions for each turbine) and transition costs between different configurations.
- Increased the flexibility of the combined-cycle units in terms of unit commitment.
- Explored the structure of the state transition graph for combined-cycle units (such as the network flow structure) that commercial optimization solvers, e.g., CPLEX, can recognize.

# Strengthened Edge-Based Combined-Cycle Unit Model

## ■ Motivation

- Reduce the computational time in the day-ahead unit commitment engine caused by combined-cycle units.

## ■ Method

- Cutting plane method.

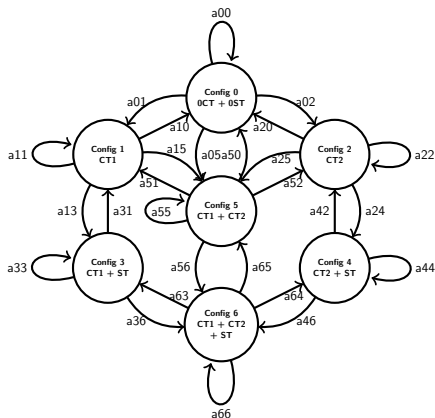
## ■ Contribution

- Derived tighter min-up/-down and ramping rate constraints for a combined-cycle unit.
- Provided several families of stronger valid inequalities of ramping rates for a combined-cycle unit by exploring the structure of the transition graph.

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# Transition Graph



- Use complete transition graph (distinguish two CTs).
- Edge binary variables ( $z_t^a$ ): transition action at each time period.
- Unique constraints:

$$\sum_{a \in \mathcal{A}} z_t^a = 1, \forall t. \quad (1)$$

Figure: Complete Transition Graph for 2CTs + 1ST

# Network Flow

## Configuration Status

$$\sum_{a \in (\mathcal{A}_k^{\text{in}} \cup \mathcal{A}_k^{\text{sl}})} z_t^a \quad (2)$$

## Logical Constraints

$$\sum_{a \in (\mathcal{A}_k^{\text{in}} \cup \mathcal{A}_k^{\text{sl}})} z_t^a = \sum_{a \in (\mathcal{A}_k^{\text{out}} \cup \mathcal{A}_k^{\text{sl}})} z_{t+1}^a, \forall k \in \mathcal{C}, \forall t. \quad (3)$$

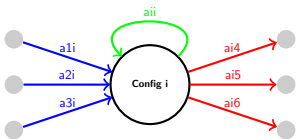
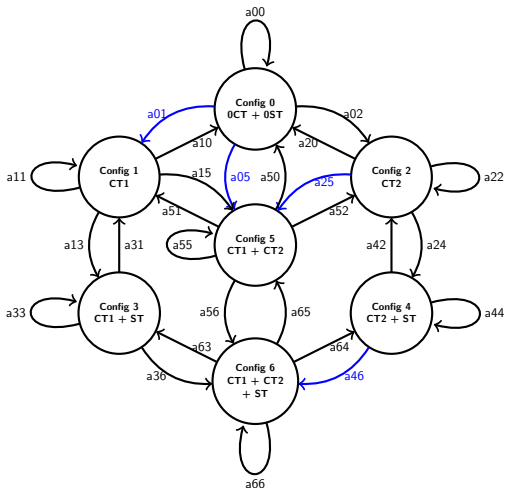


Figure: Edges of One Node

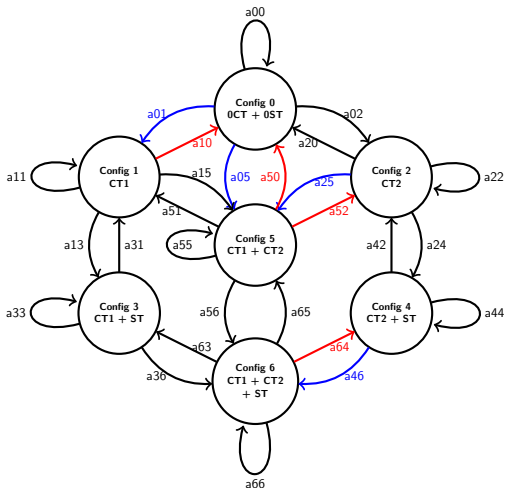
# Min-up Time



- CT1 Starts up:  
 $a_{01}$ ,  $a_{05}$ ,  $a_{25}$ ,  $a_{46}$

Figure: Start-up CT1

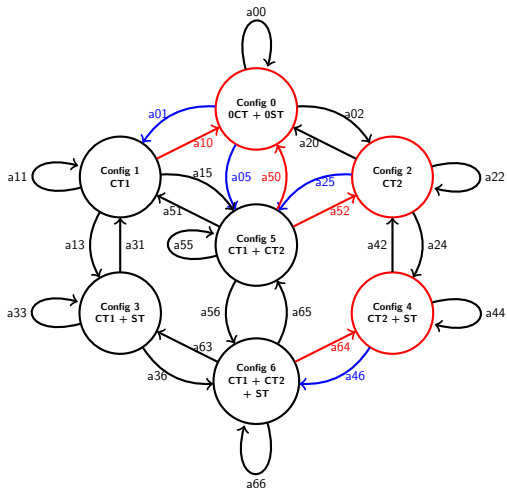
# Min-up Time



- CT1 starts up:  
a01, a05, a25, a46
- CT1 cannot shut down:  
a10, a50, a52, a64

Figure: Start-up CT1

# Min-up Time

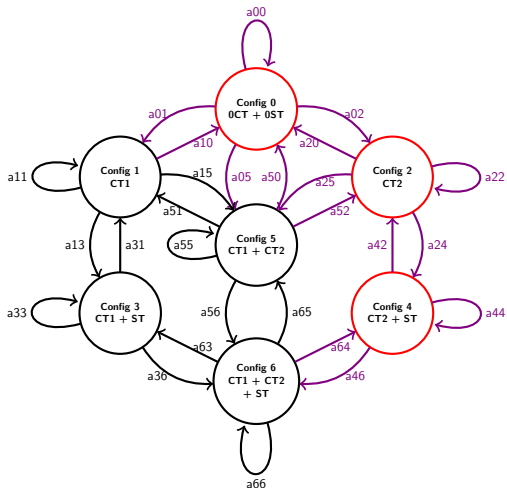


- CT1 starts up:  
a01, a05, a25, a46
- CT1 cannot shut down:  
a10, a50, a52, a64
- Configurations without CT1 cannot be online:  
Config 0, Config 2, Config 4

Figure: Start-up CT1



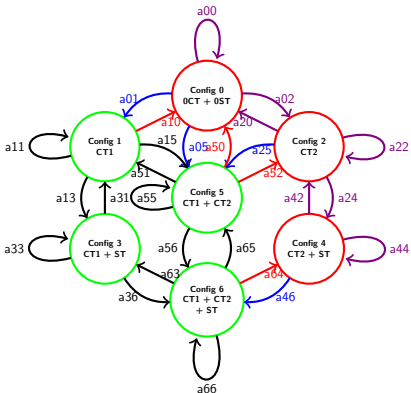
# Min-up Time



- CT1 starts up:  
 $a_{01}$ ,  $a_{05}$ ,  $a_{25}$ ,  $a_{46}$
- CT1 cannot shut down:  
 $a_{10}$ ,  $a_{50}$ ,  $a_{52}$ ,  $a_{64}$
- Configurations without CT1 cannot be online:  
Config 0, Config 2, Config 4
- Edges connected with Red configurations cannot be active.

Figure: Start-up CT1

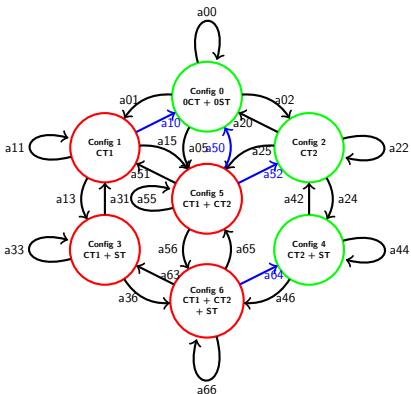
# Min-up Time Constraints



$$\sum_{a \in \bigcup_{k \in \mathcal{C}^{\text{off}}} \mathcal{A}_k^{\text{all}}} z_t^a \leq 1 - \sum_{a \in \mathcal{A}_i^{\text{su}}} z_t^a, \forall i \in \mathcal{U}^{\text{CT}} \cup \mathcal{U}^{\text{ST}},$$

$$\forall \tau \in \{t + 1, \dots, \min\{\mathcal{T}_{\text{end}}, T_{\text{mu}}^i + t - 1\}\}, \forall t. \quad (4)$$

# Min-down Time Constraints



$$\sum_{a \in \bigcup_{k \in \mathcal{C}} \mathcal{A}_k^{\text{all}}} z_{\tau}^a \leq 1 - \sum_{a \in \mathcal{A}_i^{\text{sd}}} z_t^a, \forall i \in \mathcal{U}^{\text{CT}} \cup \mathcal{U}^{\text{ST}},$$

$$\tau \in \{t + 1, \dots, \min\{\mathcal{T}_{\text{end}}, T_{\text{md}}^i + t - 1\}\}, \forall t. \quad (5)$$

# Ramping Constraints

- If this particular edge is not active (i.e.,  $z_{t+1}^a = 0$ ), this ramping constraint is relaxed, following the definition of  $P^{\text{cap}}$
- Otherwise, if this edge is active (i.e.,  $z_{t+1}^a = 1$ ), this edge provides the ramping limit for the whole combined-cycle unit, because only one of the edges can be active at each time period.

$$p_{t+1} - p_t \leq RU_a z_{t+1}^a + P^{\text{cap}}(1 - z_{t+1}^a), \forall a \in \mathcal{A}, \forall t, \quad (6)$$

$$p_t - p_{t+1} \leq RD_a z_{t+1}^a + P^{\text{cap}}(1 - z_{t+1}^a), \forall a \in \mathcal{A}, \forall t. \quad (7)$$

# Reduced State Transition Graph

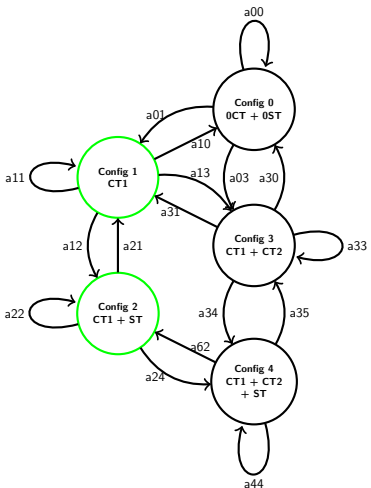


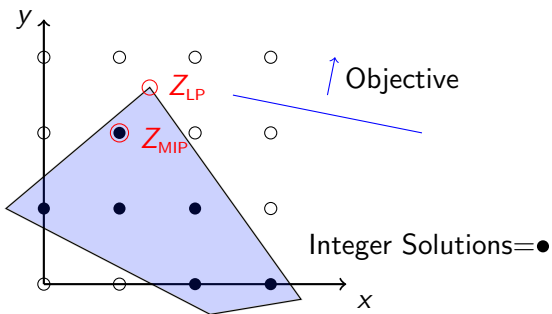
Figure: Reduced State Transition Graph for 2CT+1ST

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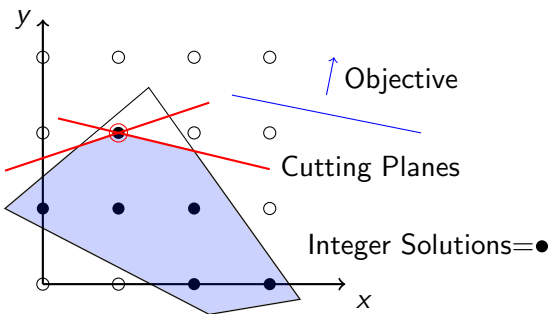
# Cutting Planes

Strong valid inequalities to cut off fractional solutions.



# Cutting Planes

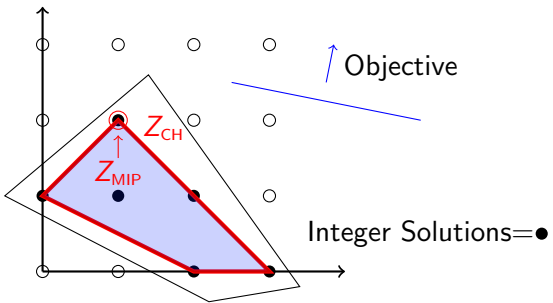
Strong valid inequalities to cut off fractional solutions.





# Convex Hull

The smallest convex feasible region containing all feasible integer solutions



# Min-up Time Constraints

- If turbine  $i$  is online at time period  $t$ , then this turbine starts up at most once during time interval  $[t - T_{\text{mu}}^i + 1, t - 1]$ .
- If turbine  $i$  starts up at time interval  $[t - T_{\text{mu}}^i + 1, t - 1]$ , then the configurations without turbine  $i$  cannot be online at time period  $t$ .

$$\sum_{\kappa=1}^{T_{\text{mu}}^i-1} \sum_{a \in \mathcal{A}_i^{\text{su}}} z_{t-\kappa}^a \leq 1 - \sum_{a \in \bigcup_{k \in \mathcal{C}_i^{\text{off}}} \mathcal{A}_k^{\text{all}}} z_t^a, \quad (8)$$
$$\forall i \in \mathcal{U}^{\text{CT}} \cup \mathcal{U}^{\text{ST}}, \forall t \in \{T_{\text{mu}}^i, \dots, T_{\text{end}}\}.$$

# Min-down Time Constraints

- If one of the arcs in  $\mathcal{A}_{sd}^i$ , representing the shut-down process of turbine  $i$ , is active during time interval  $[t - T_{md}^i + 1, t - 1]$ , then arcs  $\bigcup_{k \in \mathcal{C}_i^{on}} \mathcal{A}_k^{all}$  connected to the configurations ( $\mathcal{C}_i^{on}$ ) with turbine  $i$  cannot be active.
- The configurations with turbine  $i$  must be offline at time period  $t$  when turbine  $i$  shuts down at time interval  $[t - T_{md}^i + 1, t - 1]$ .

$$\sum_{\kappa=1}^{T_{md}^i-1} \sum_{a \in \mathcal{A}_i^{sd}} z_{t-\kappa}^a \leq 1 - \sum_{a \in \bigcup_{k \in \mathcal{C}_i^{on}} \mathcal{A}_k^{all}} z_t^a,$$

$$\forall i \in \mathcal{U}^{CT} \cup \mathcal{U}^{ST}, \forall t \in \{T_{md}^i, \dots, T_{end}\}. \quad (9)$$

# Ramping Rate Constraints

- Since only one of the arcs in the transition graph can be active at each time period  $t$ , only one item in the right-hand side of (10) can be positive and all others would be zeros.
- The positive item represents the active arc that provides the ramping up rate limit. The same analysis can be applied to ramping down constraints (11)

$$p_{t+1} - p_t \leq \sum_{a \in \mathcal{A}} RU_a z_{t+1}^a, \forall t \in \mathcal{T}, \quad (10)$$

$$p_t - p_{t+1} \leq \sum_{a \in \mathcal{A}} RD_a z_{t+1}^a, \forall t \in \mathcal{T}. \quad (11)$$

# Single-Arc Ramping Up Rate Inequalities

$$\begin{aligned}
 p_{t+1}^m - p_t^n &\leq \text{RU}^{a(n,m)} z_{t+1}^{a(n,m)} + \overline{P}_m \left( \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a \right) \\
 &\quad - \underline{P}_n \left( \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a \right) + (\underline{P}_n - \overline{P}_m) z_{t+1}^{a(n,m)}, \\
 \forall a(n, m) \in \mathcal{A}, \forall t \in \mathcal{T},
 \end{aligned} \tag{12}$$

Table: Validity of Ramping Up Inequalities (12)

Case	Value of Binary Variables			Inequality	
	$\sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a$	$\sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a$	$z_{t+1}^{a(n,m)}$	LHS	RHS
1	1	1	1	$p_{t+1}^m - p_t^n$	$\text{RU}^{a(n,m)}$
2	1	0	0	$-p_t^n$	$-\underline{P}_n$
3	0	1	0	$p_{t+1}^m$	$\overline{P}_m$
4	0	0	0	0	0

# Single-Arc Ramping Down Rate Inequalities

$$\begin{aligned}
 p_t^n - p_{t+1}^m &\leq \text{RD}^{a(n,m)} z_{t+1}^{a(n,m)} + \overline{P}_n \left( \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a \right) \\
 &\quad - \underline{P}_m \left( \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a \right) + (\underline{P}_m - \overline{P}_n) z_{t+1}^{a(n,m)}, \\
 \forall a(n, m) \in \mathcal{A}, \forall t \in \mathcal{T}.
 \end{aligned} \tag{13}$$

Table: Validity of Ramping Down Inequalities (13)

Case	Value of Binary Variables			Inequality	
	$\sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a$	$\sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a$	$z_{t+1}^{a(n,m)}$	LHS	RHS
1	1	1	1	$p_t^n - p_{t+1}^m$	$\text{RD}^{a(n,m)}$
2	1	0	0	$p_t^n$	$\overline{P}_n$
3	0	1	0	$-p_{t+1}^m$	$-\underline{P}_m$
4	0	0	0	0	0

# Multi-Configuration Ramping Rate Inequalities

- Suppose that the combined-cycle unit works on Configuration  $m$  at time period  $t + 1$ . As shown in the following figure, we know one of the incoming arcs ( $a_{n_1,m}$ ,  $a_{n_2,m}$ ,  $a_{n_3,m}$ ) or the self-loop arc  $a_{m,m}$  must be active at time period  $t + 1$ .

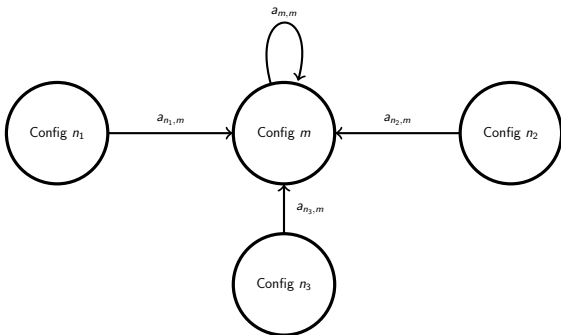


Figure: Configuration Transition Graph for Configuration  $m$

# Multi-Configuration Ramping Up Rate Inequalities

$$\begin{aligned}
 p_{t+1}^m - \sum_{n \in \mathcal{C} \rightarrow m} p_t^n &\leq \sum_{n \in \mathcal{C} \rightarrow m} \text{RU}^{a(n,m)} z_{t+1}^{a(n,m)} \\
 &- \sum_{n \in \mathcal{C} \rightarrow m} \frac{P_n}{z_{t+1}^a} \left( \left( \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a \right) - z_{t+1}^{a(n,m)} \right), \forall m \in \mathcal{C}, \forall t.
 \end{aligned} \tag{14}$$

Table: Validity of Ramping Up Inequalities (14)

Case	Value of Binary Variables		Inequality	
	$\sum_{n \in \mathcal{C} \rightarrow m} z_{t+1}^{a(n,m)}$	$\sum_{n \in \mathcal{C} \rightarrow m} \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a$	LHS	RHS
1	1	1	$p_{t+1}^m - p_t^{\bar{n}}$	$\text{RU}^{a(\bar{n},m)}$
2	0	1	$-p_t^{\bar{n}}$	$-\frac{P_{\bar{n}}}{z_{t+1}^a}$
3	0	0	0	0



# Multi-Configuration Ramping Down Rate Inequalities

$$\begin{aligned}
 \sum_{n \in \mathcal{C} \rightarrow m} p_t^n - p_{t+1}^m &\leq \sum_{n \in \mathcal{C} \rightarrow m} \text{RD}^{a(n,m)} z_{t+1}^{a(n,m)} \\
 + \sum_{n \in \mathcal{C} \rightarrow m} \overline{P}_n &\left( \left( \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a \right) - z_{t+1}^{a(n,m)} \right), \forall m \in \mathcal{C}, \forall t.
 \end{aligned} \tag{15}$$

**Table:** Validity of Ramping Down Inequalities (15)

Case	Value of Binary Variables		Inequality	
	$\sum_{n \in \mathcal{C} \rightarrow m} z_{t+1}^{a(n,m)}$	$\sum_{n \in \mathcal{C} \rightarrow m} \sum_{a \in (\mathcal{A}_n^{\text{in}} \cup \mathcal{A}_n^{\text{sl}})} z_t^a$	LHS	RHS
1	1	1	$p_t^{\bar{n}} - p_{t+1}^m$	$\text{RD}^{a(\bar{n},m)}$
2	0	1	$p_t^{\bar{n}}$	$\overline{P}_{\bar{n}}$
3	0	0	0	0

# Multi-Configuration Ramping Rate Inequalities

- Suppose that the combined-cycle unit works on Configuration  $n$  at time period  $t$  in the following figure. Then, one of the outgoing arcs  $(a_{n,m_1}, a_{n,m_2}, a_{n,m_3})$  or the self-loop arc  $a_{n,n}$  must be active at time period  $t + 1$ .

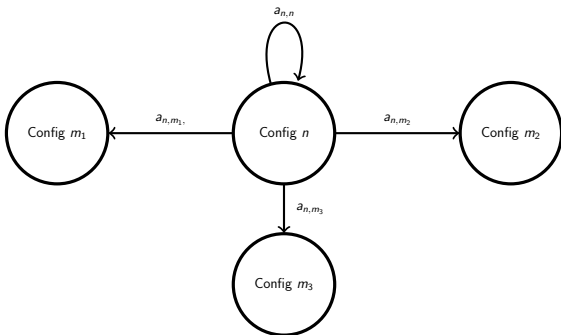


Figure: Configuration Transition Graph for Configuration  $n$

# Multi-Configuration Ramping Up Rate Inequalities

$$\sum_{m \in \mathcal{C}_{n \rightarrow}} p_{t+1}^m - p_t^n \leq \sum_{m \in \mathcal{C}_{n \rightarrow}} \text{RU}^{a(n,m)} z_{t+1}^{a(n,m)} \quad (16)$$

$$+ \sum_{m \in \mathcal{C}_{n \rightarrow}} \bar{P}_m \left( \left( \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a \right) - z_{t+1}^{a(n,m)} \right), \forall n \in \mathcal{C}, \forall t.$$

Table: Validity of Ramping Up Inequalities (16)

Case	Value of Binary Variables		Inequality	
	$\sum_{m \in \mathcal{C}_{n \rightarrow}} z_{t+1}^{a(n,m)}$	$\sum_{m \in \mathcal{C}_{n \rightarrow}} \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a$	LHS	RHS
1	1	1	$p_{t+1}^{\bar{m}} - p_t^n$	$\text{RU}^{a(n,\bar{m})}$
2	0	1	$p_t^{\bar{m}}$	$\bar{P}_{\bar{m}}$
3	0	0	0	0

# Multi-Configuration Ramping Down Rate Inequalities

$$\begin{aligned}
 p_n^t - \sum_{m \in \mathcal{C}_{n \rightarrow}} p_{t+1}^m &\leq \sum_{m \in \mathcal{C}_{n \rightarrow}} \text{RD}^{a(n,m)} z_{t+1}^{a(n,m)} \\
 - \sum_{m \in \mathcal{C}_{n \rightarrow}} \frac{P_m}{P_n} &\left( \left( \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a \right) - z_{t+1}^{a(n,m)} \right), \forall n \in \mathcal{C}, \forall t.
 \end{aligned} \tag{17}$$

**Table:** Validity of Ramping Down Inequalities (17)

Case	Value of Binary Variables		Inequality	
	$\sum_{m \in \mathcal{C}_{n \rightarrow}} z_{t+1}^{a(n,m)}$	$\sum_{m \in \mathcal{C}_{n \rightarrow}} \sum_{a \in (\mathcal{A}_m^{\text{in}} \cup \mathcal{A}_m^{\text{sl}})} z_{t+1}^a$	LHS	RHS
1	1	1	$p_t^n - p_{t+1}^{\bar{m}}$	$\text{RD}^{a(n,\bar{m})}$
2	0	1	$-p_t^{\bar{m}}$	$-\frac{P_{\bar{m}}}{P_n}$
3	0	0	0	0

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# Experiment Setting

- IEEE 118 Bus System: 54 traditional thermal units and 12 combined-cycle units.
- 10 different load scenarios.
- Intel(R) Core(TM) i7-4500U 1.8GHz with 8G memory and CPLEX 12.5.
- EBF: Edge-based formulation.
- TEBF: The edge-based formulation with min-up/-down constraints (4) and (5) replaced by tighter min-up/-down constraints (8) and (9).
- REBF: The edge-based formulation with ramping constraints (6) and (7) replaced by tighter ramping constraints (10) - (17).
- SEBF: Strengthened edge-based formulation.

# Computational Results

Table: Root Node Information

Cases		LP Objective Values (\$)				Integrality Gap ( $10^{-4}$ )			
		EBF	TEBF	REBF	SEBF	EBF	TEBF	REBF	SEBF
G-I	1	1879876	1880212	1880451	1880774	9.92	8.11	6.85	5.14
	2	1879103	1879456	1879698	1880031	10.15	8.30	7.10	5.34
	3	1885160	1885489	1885739	1886056	10.01	8.29	6.93	5.26
	4	1876169	1876512	1876746	1877070	10.01	8.19	6.96	5.15
	5	1887136	1887470	1887715	1888032	9.39	7.84	6.53	4.74
G-II	1	3615129	3615571	3616036	3616440	9.18	8.08	6.90	6.68
	2	3606929	3607372	3607865	3608274	9.98	7.72	6.68	6.05
	3	3602757	3603224	3603670	3604094	11.47	8.79	7.30	6.2
	4	3609224	3609688	3610134	3610562	9.89	9.09	7.34	6.75
	5	3607151	3607576	3608070	3608472	11.45	9.25	7.89	6.17

# Computational Results

Table: Computational Times

Cases		Time				Number of Nodes			
		EBF	TEBF	REBF	SEBF	EBF	TEBF	REBF	SEBF
G-I	1	1668.92	1478.32	1208.08	650.23	4526	3315	2537	1064
	2	1383.41	985.74	538.77	604.61	4570	2562	644	828
	3	1474.76	1569.19	483.59	400.15	3683	5895	1218	952
	4	1282.29	903.13	502.99	335.69	2899	2471	640	442
	5	1240.13	811.17	317.38	407.5	4375	2154	299	572
G-II	1	1114.08	945.24	999.92	797.65	1184	1197	377	316
	2	***	884.34	489.7	666.86	1206	1248	0	0
	3	***	***	833.12	828.68	1213	1190	174	126
	4	2512.31	3411.7	1820.3	798.59	1251	1233	1134	204
	5	***	3231.19	702.01	834.63	1157	1486	0	152



# Convergence Process

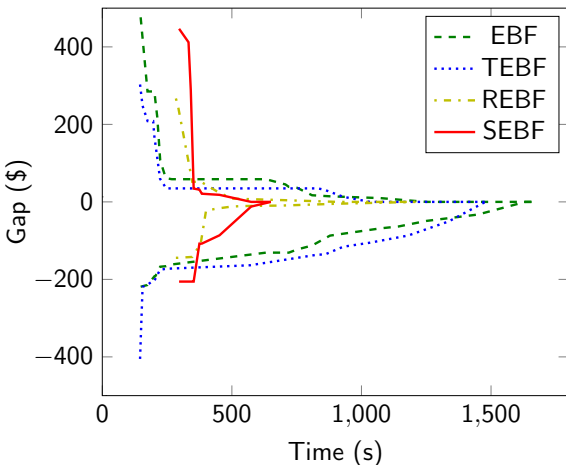


Figure: Convergence evolution of Case 1 in One-Day UC

# Convergence Process

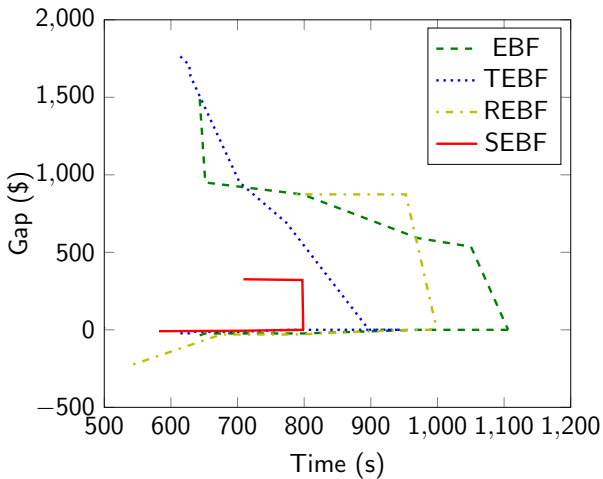


Figure: Convergence evolution of Case 1 in Two-Day UC

# Outline

- 1 Introduction
  - Introduction
  - Motivation
- 2 Edge-Based Formulation
  - Transition Graph Representation
  - Operating Constraints
- 3 Strengthened Edge-Based Formulation
  - Tighter Constraints
  - Strong Valid Inequalities
- 4 Case Studies
- 5 Conclusion

# Contributions

- Increase the accuracy. Exactly describe the physical constraints (in particular, min-up/-down restrictions for each turbine) and transition costs between different configurations.
- Increase the flexibility by tracking the status of each turbine.
- A better computational performance.

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# Q&A

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Thank you!